



TRANSPORT CANADA Delegates Conference Ottawa, November 14-15, 2018

EPICEA R&D project

DR Fidele Moupfouma
(PHD in Engineering &
Doctor of Sciences in Physics)

Principal Engineer Specialist
Electromagnetic domain Knowledge Owner

Bombardier Aerospace
Strategic Technologies & Innovation

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AGENDA

➤ ELECTROMAGNETIC COUPLING MECHANISM IN COMPOSITE # METALLIC AIRCRAFT

- Aircraft Structure Skin Effect
- Lightning Indirect Effects on Systems
- Signal Return Network Contribution
- Systems` Susceptibility
- Emissions

➤ EPICEA

- EPICEA COLLABORATIVE TEAM
- Rational and Trend → why we need EPICEA?
- Description of the EPICEA test barrel structure;
- EM Testing – Sample results for LIE;
- EM Modeling – Barrel model generation;
- Harness test data analysis
- Conclusion

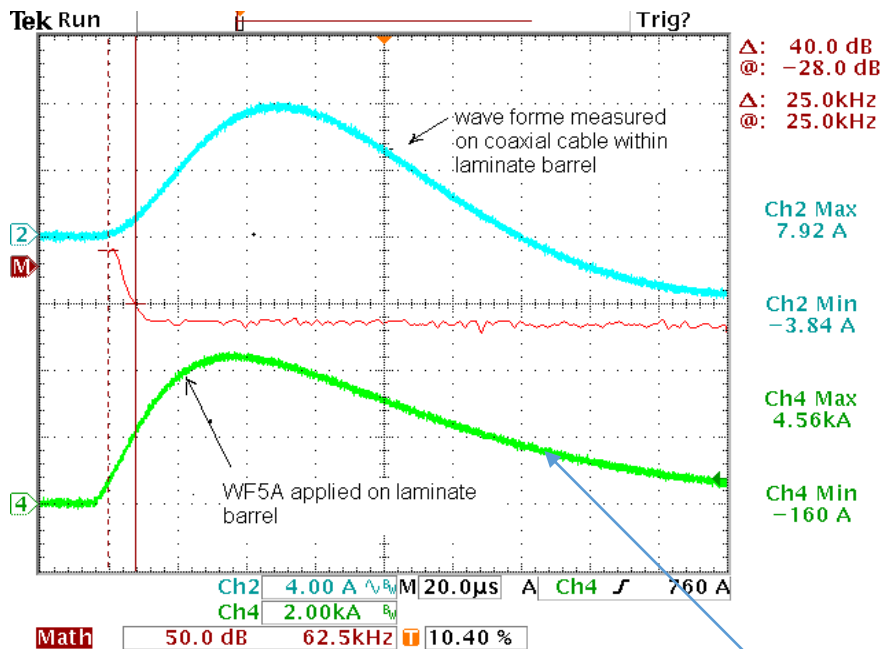
AIRCRAFT STRUCTURE SKIN EFFECT

- ❑ In an Electromagnetic Environment , the aircraft structure is governed by its electrical parameters : **Conductivity σ** and **Permeability μ**
- ❑ Skin Effect : $\delta = \frac{1}{\sqrt{\mu\sigma f}}$
- ❑ Due to the structure skin effect δ , lightning current will propagate on the structure for some time τ_s , before penetrating the skin (governed by a thickness **T**) by induction and coupling to cables inside the aircraft

$$\tau_s = \frac{1}{\pi f} \times \left(\frac{T}{\delta} \right)^2 = \mu_o \sigma T^2$$

LIGHTNING-INDUCED CURRENT ON CABLE SHIELD

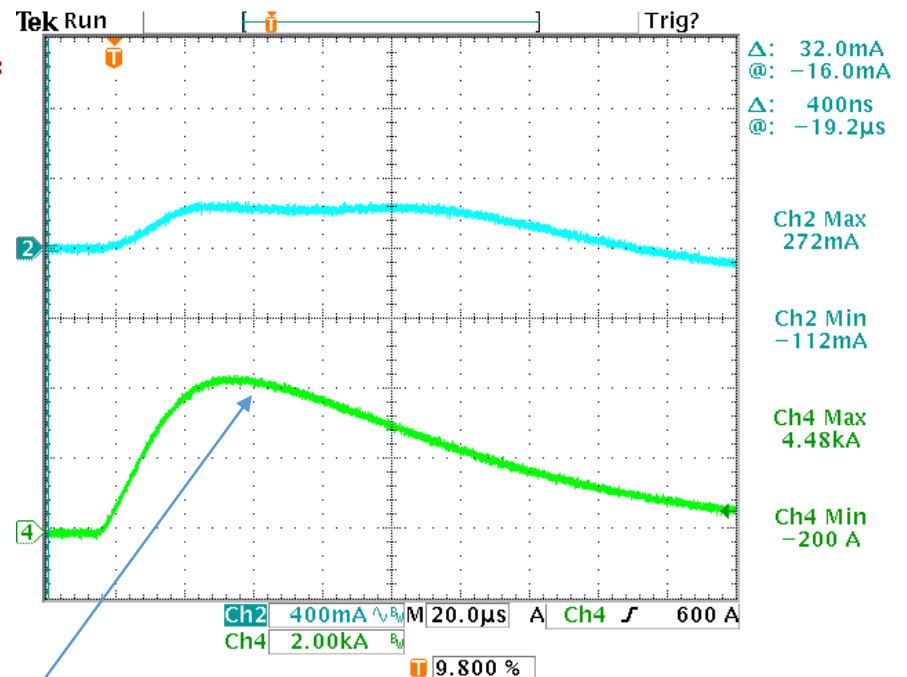
Common MODE SYSTEM BEHAVIOR (WF5 lightning environment)



Coaxial cable current
measured in composite barrel

Lightning Energy
Applied to composite &
Metallic barrel

σ

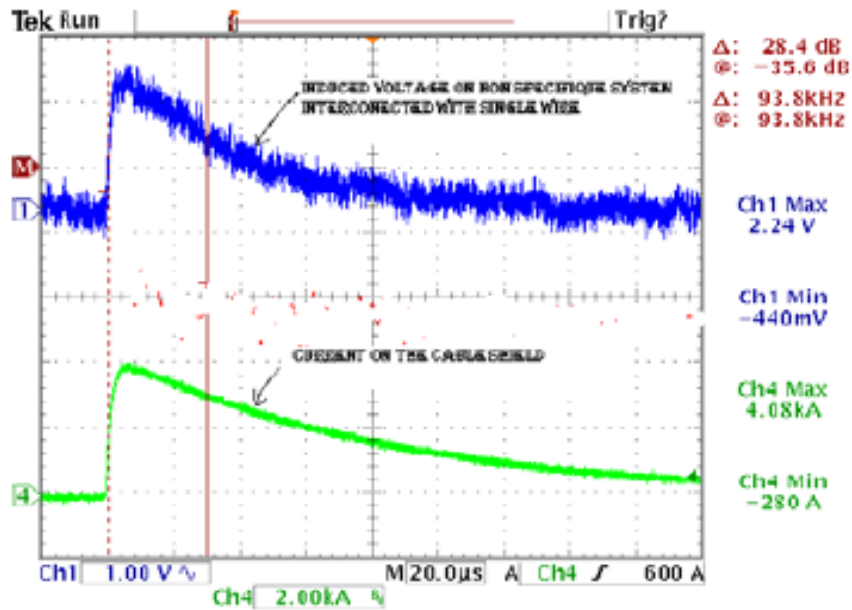


Coaxial cable current
measured in aluminum barrel

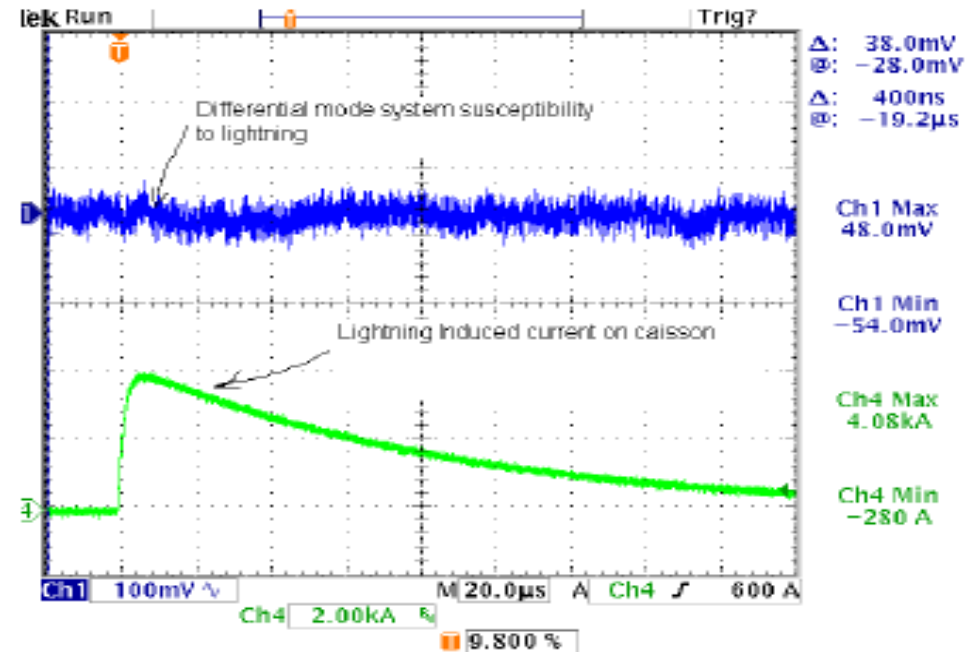
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LIGHTNING-INDUCED CURRENT ON CABLE SHIELD

Differential MODE SYSTEM BEHAVIOR (WF1 lightning environment)



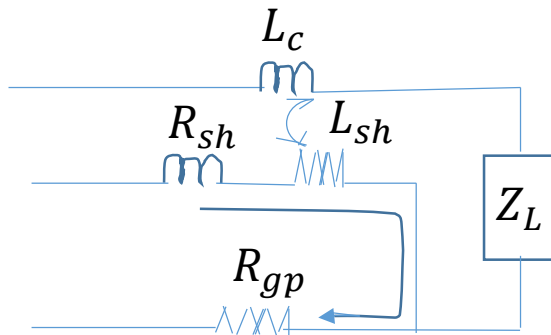
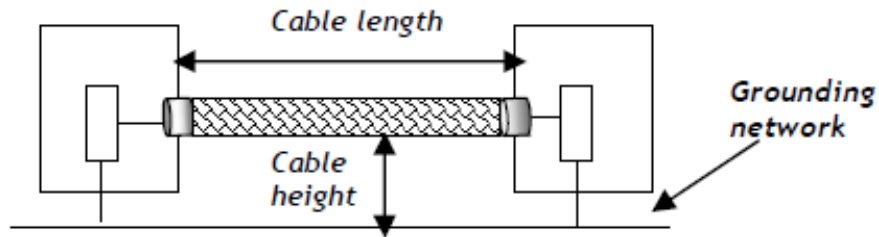
Composite barrel



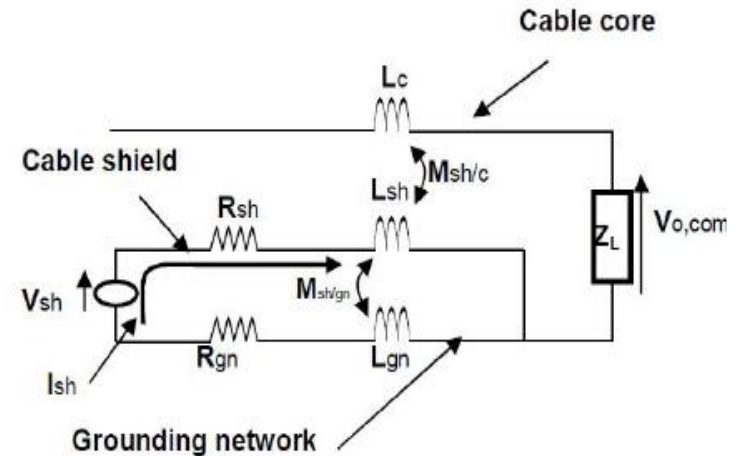
Metallic barrel

SIGNAL RETURN NETWORK CONTRIBUTION

DISSIMILARITY OF ELECTROMAGNETIC COUPLING MECHANISM Between Composite and Metallic Aircraft



Kirchoff circuitry on
metallic aircraft



Kirchoff circuitry on
composite aircraft

SYSTEMS SUSCEPTIBILITY ASSESSMENT

- ✓ EM. voltage at a system level on a metallic aircraft

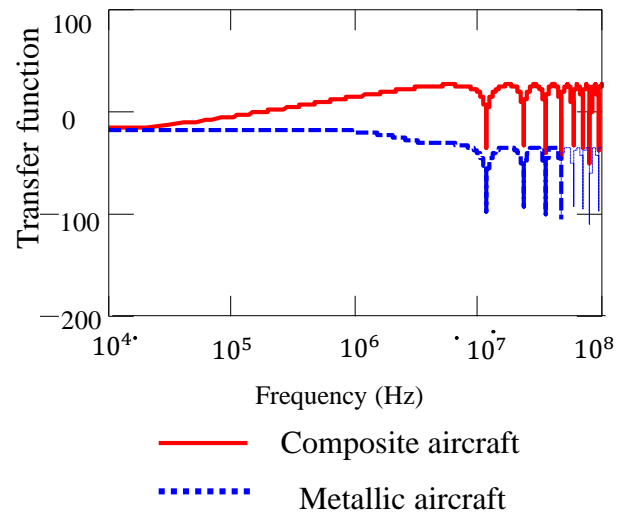
$$V(f) = I_o \times \frac{length}{2} [Z_T(f) - Z_o Y_T(f) Z_{bd}] \times \exp\left(-j\pi\sqrt{\epsilon_r} \frac{length}{\lambda}\right) \times \frac{\sin\left((\sqrt{\epsilon_r} - 1)\pi \frac{length}{\lambda}\right)}{\left((\sqrt{\epsilon_r} - 1)\pi \frac{length}{\lambda}\right)}$$

- ✓ EM. voltage at a system level on a composite aircraft

$$V(f) = I_o \frac{length}{2} \exp\left(-j\frac{\pi}{\lambda} \sqrt{\epsilon_r} length\right) \left((Z_t(f) - j2\pi f M_{shg}) - Z_{bd} Z_o Y_T(f) \right) \\ \times \frac{\sin\left[\frac{\pi (\sqrt{\epsilon_r} - 1)}{\lambda} length\right]}{\frac{\pi (\sqrt{\epsilon_r} - 1)}{\lambda} length}$$

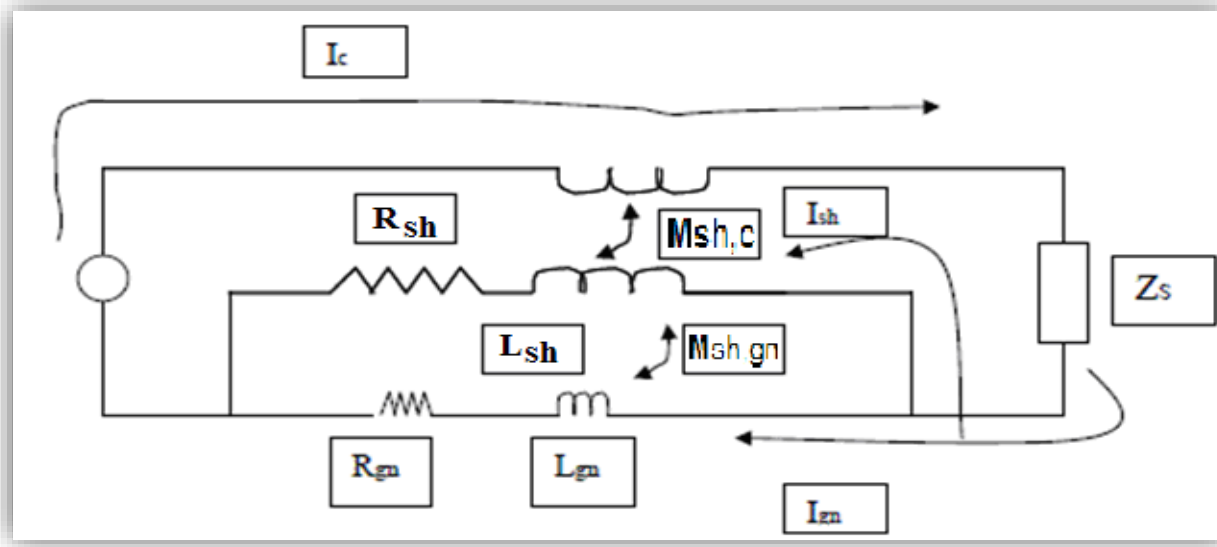
TRANSFER FUNCTION

Comparison Composite # Metallic Aircraft



SPECTRAL COMPARISON OF EMISSIONS BY CONDUCTION DUE TO HARNESSSES

Emissions at low frequencies are due to the magnetic field that is frequency dependent. Due to the SRN coupling with harnesses, those emission are higher on composite than on metallic aircraft



SPECTRAL COMPARISON OF EMISSIONS BY CONDUCTION DUE TO CABLES

✓ Composite Aircraft

$$\frac{I_{sh}}{I_C} = \frac{(L_{gn} - M_{sh\ gn} + M_{sh\ c})}{(L_{sh} - M_{sh\ gn}) + (L_{gn} - M_{sh\ gn})} \left\{ \frac{\left[j\omega + \frac{R_{gn}}{(L_{gn} - M_{sh\ gn} + M_{sh\ c})} \right]}{\left[j\omega + \frac{(R_{gn} + R_{sh})}{(L_{sh} - M_{sh\ gn}) + (L_{gn} - M_{sh\ gn})} \right]} \right\} \quad (a)$$

✓ Metallic Aircraft

$$\frac{I_{sh}}{I_C} = \frac{R_{st} + jM_{shc}}{(R_{st} + R_{sh}) + jL_{sh}} \quad (b)$$

SPECTRAL COMPARISON OF EMISSIONS BY CONDUCTION DUE TO HARNESSES

Composite # Metallic aircraft

✓ Composite

$$\omega_c = \frac{(R_{gn} + R_{sh})}{(L_{sh} - M_{sh\ gn}) + (L_{gn} - M_{sh\ gn})}$$

(a)

Then for
 $\omega \ll \omega_c$

$$\frac{I_{sh}}{I_c} \xrightarrow{\omega \rightarrow 0} \frac{R_{gn}}{R_{sh} + R_{gn}}$$

(b)

Then for
 $\omega_c \ll \omega$

$$\frac{I_{sh}}{I_c} = \xrightarrow{\omega \rightarrow +\infty} \frac{(L_{gn} - M_{sh\ gn} + M_{sh\ c})}{(L_{sh} - M_{sh\ gn}) + (L_{gn} - M_{sh\ gn})}$$

(d)

(c)

✓ Metal

$$\omega_c = \frac{R_{st} + R_{sh}}{L_{sh}}$$

Then for
 $\omega \ll \omega_c$

$$\frac{I_{sh}}{I_c} \xrightarrow{\omega \rightarrow 0} \frac{R_{st}}{R_{sh} + R_{st}}$$

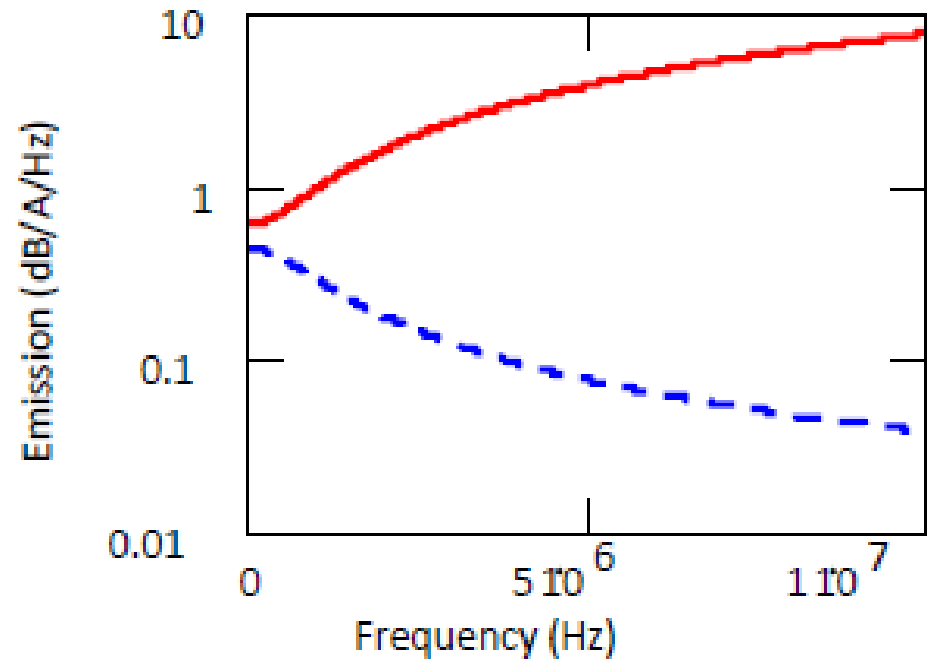
(e)

Then for
 $\omega_c \ll \omega$

$$\frac{I_{sh}}{I_c} \xrightarrow{\omega \rightarrow +\infty} \frac{M}{L_{sh}}$$

(f)

COMPARISON OF CONDUCTED EMISSIONS ON COMPOSITE METALLIC # METALLIC AIRCRAFT



Composite aircraft



Metallic aircraft



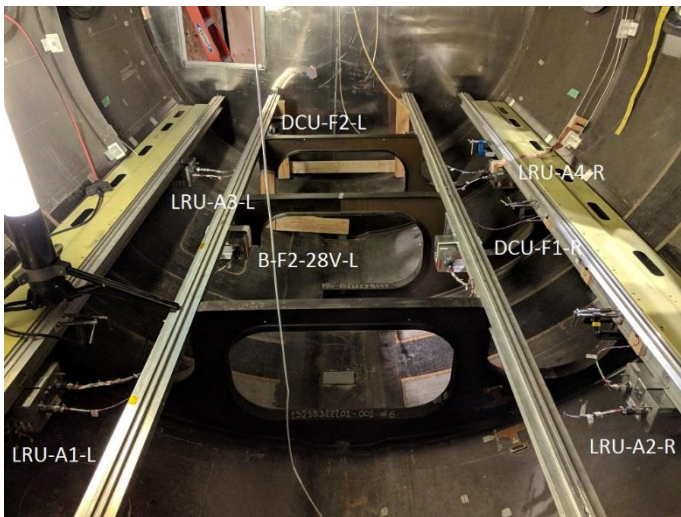
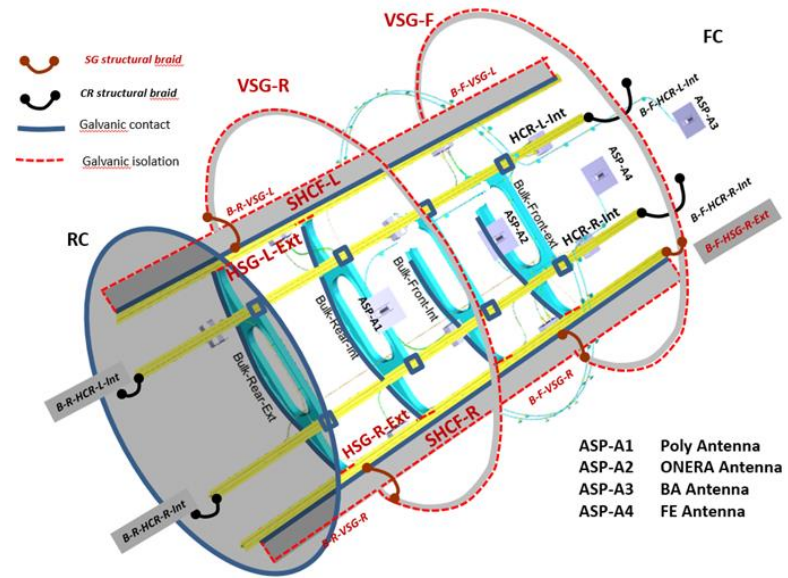
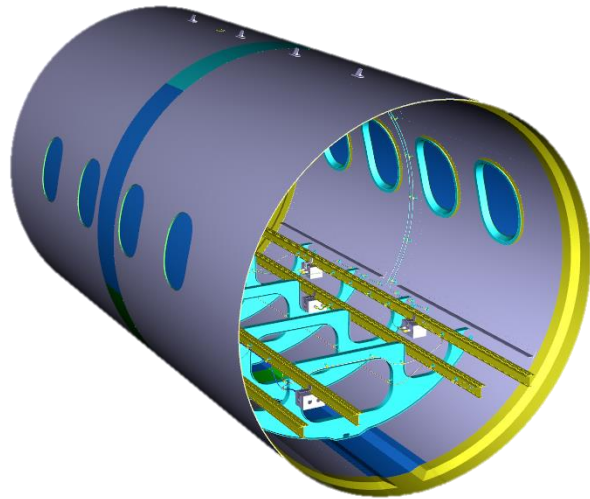
EPICEA COLLABORATIVE PROJECT



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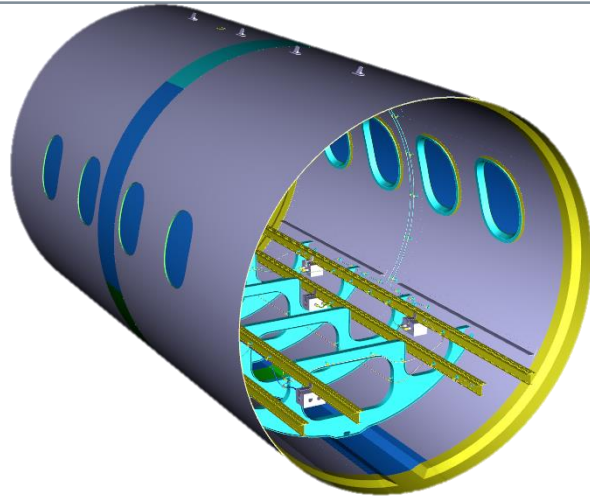
EPICEA PROJECT – Test Case

Description of the EPICEA Barrel – Structure View

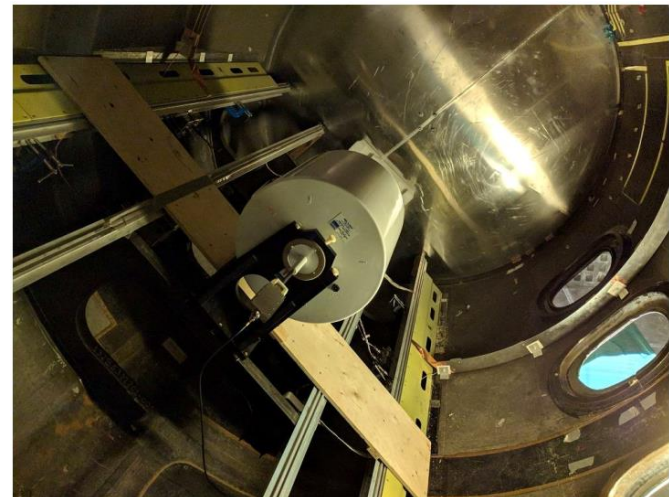
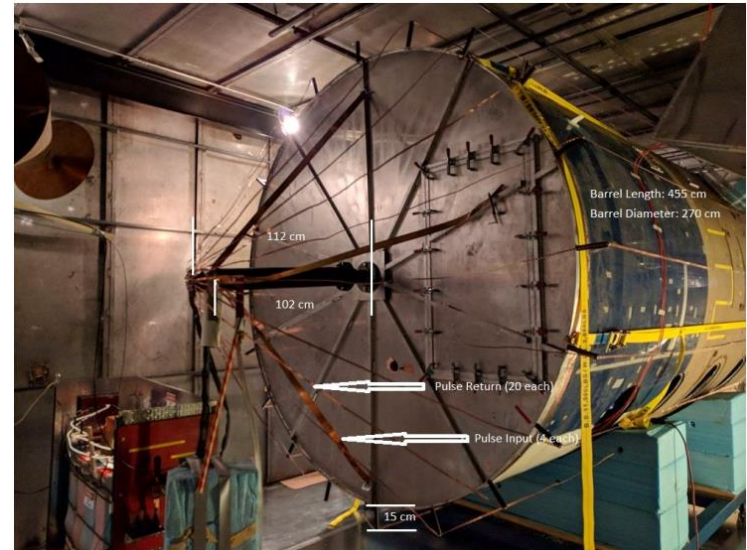
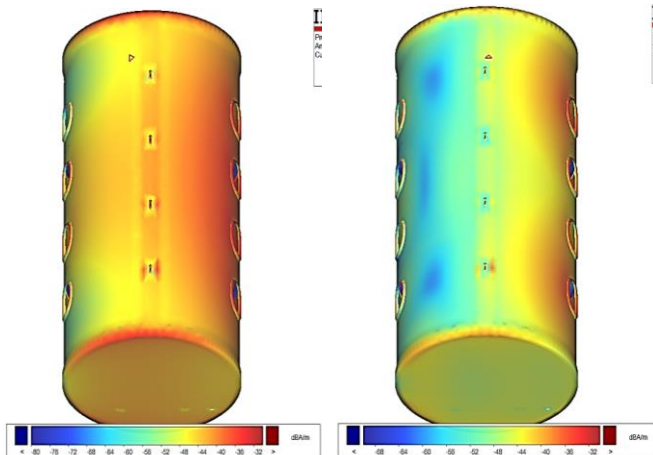


EPICEA PROJECT

LIGHTNING INDIRECT EFFECTS & HIRF TESTS

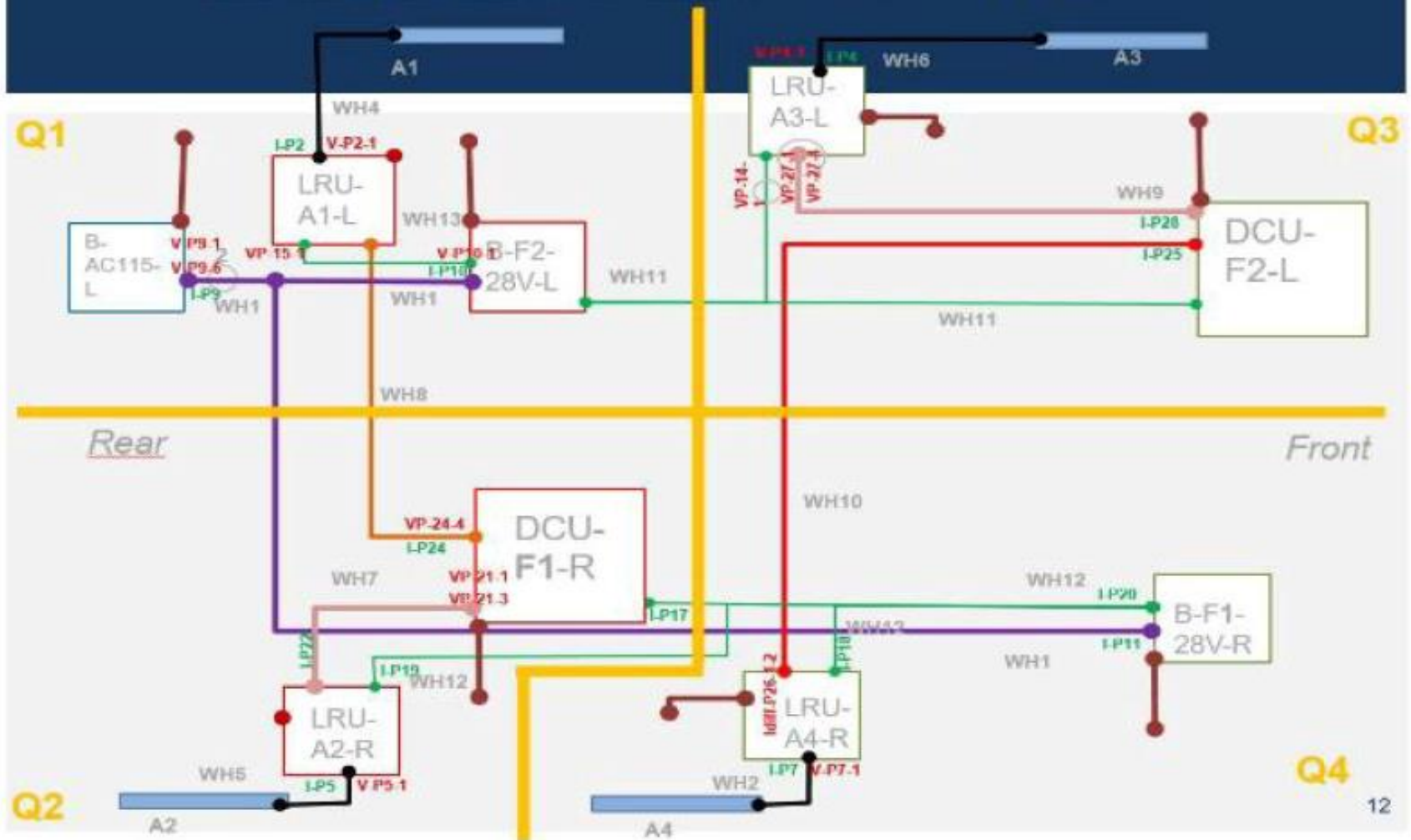


Surface current distribution @ 40 MHz and 120MHz



HARNESSES TEST FOR LIE & HIRF

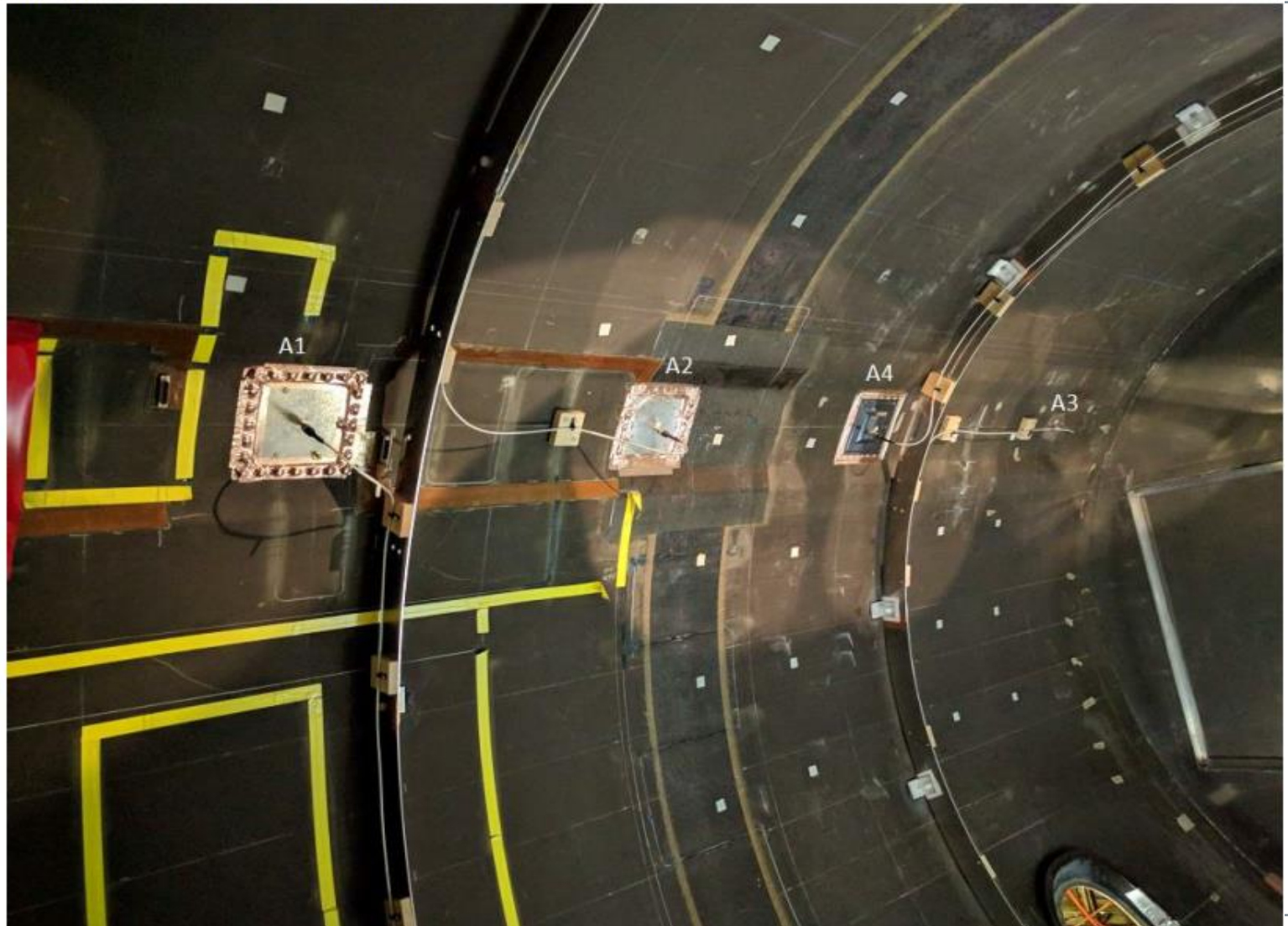
MEASUREMENT TEST POINTS



12

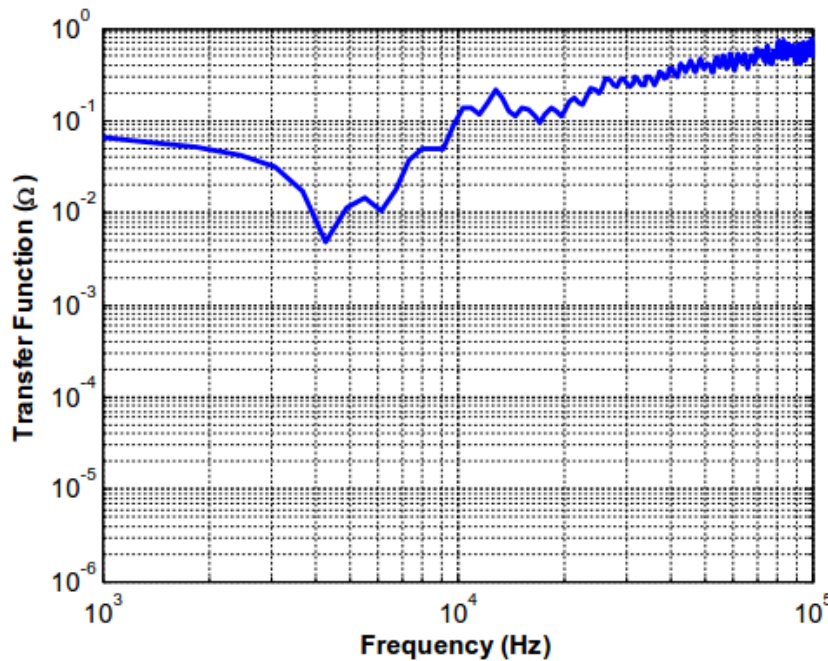
ANTENNAS INTEGRATION

Antennas marked the ground shape

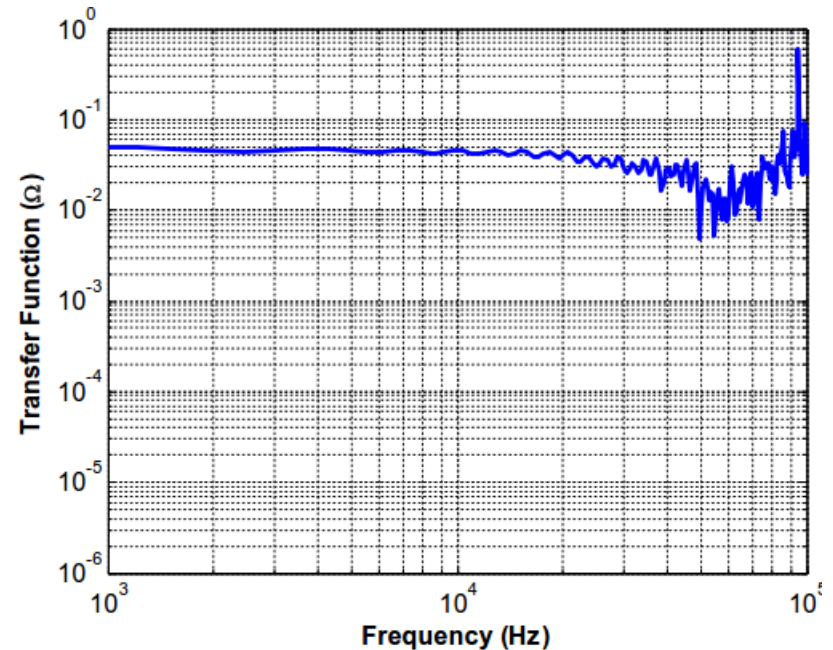


LIGHTNING INDIRECT EFFECTS

Cables Transfer Function



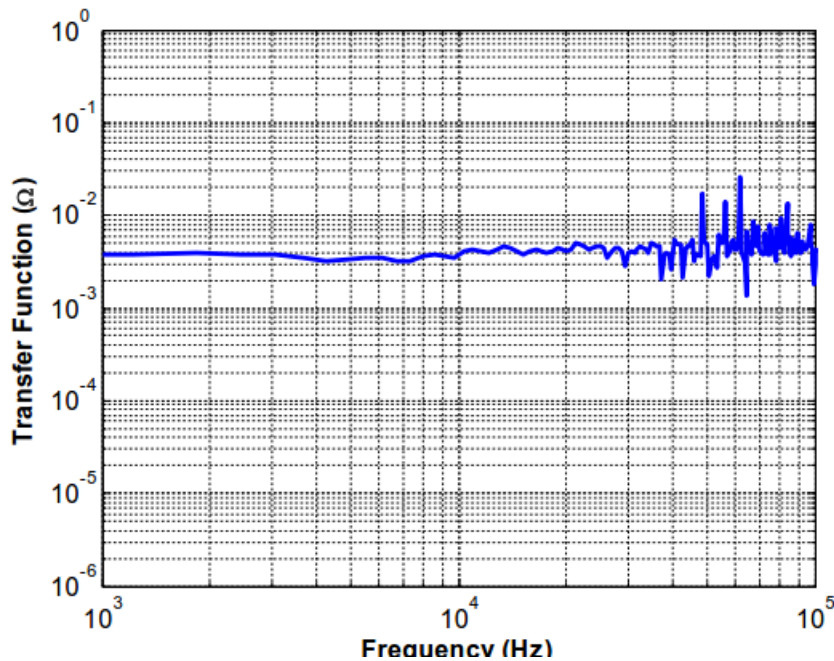
Computed Transfer Function at Test Point V P2-1
(with all bundles in WH8 Short circuited)



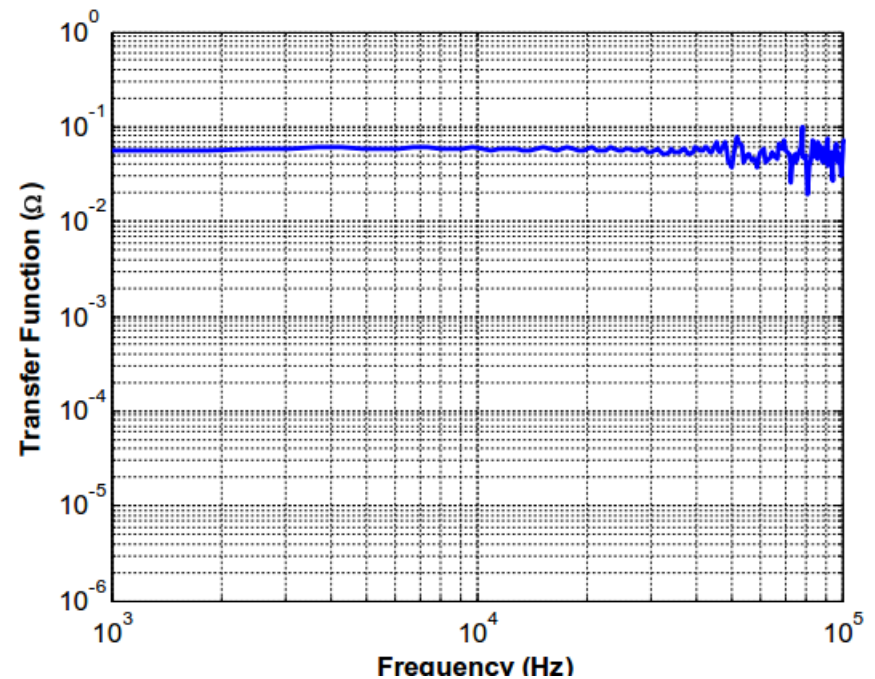
Computed Transfer Function at Test V P 4-1

LIGHTNING INDIRECT EFFECTS

Cables Transfer Function

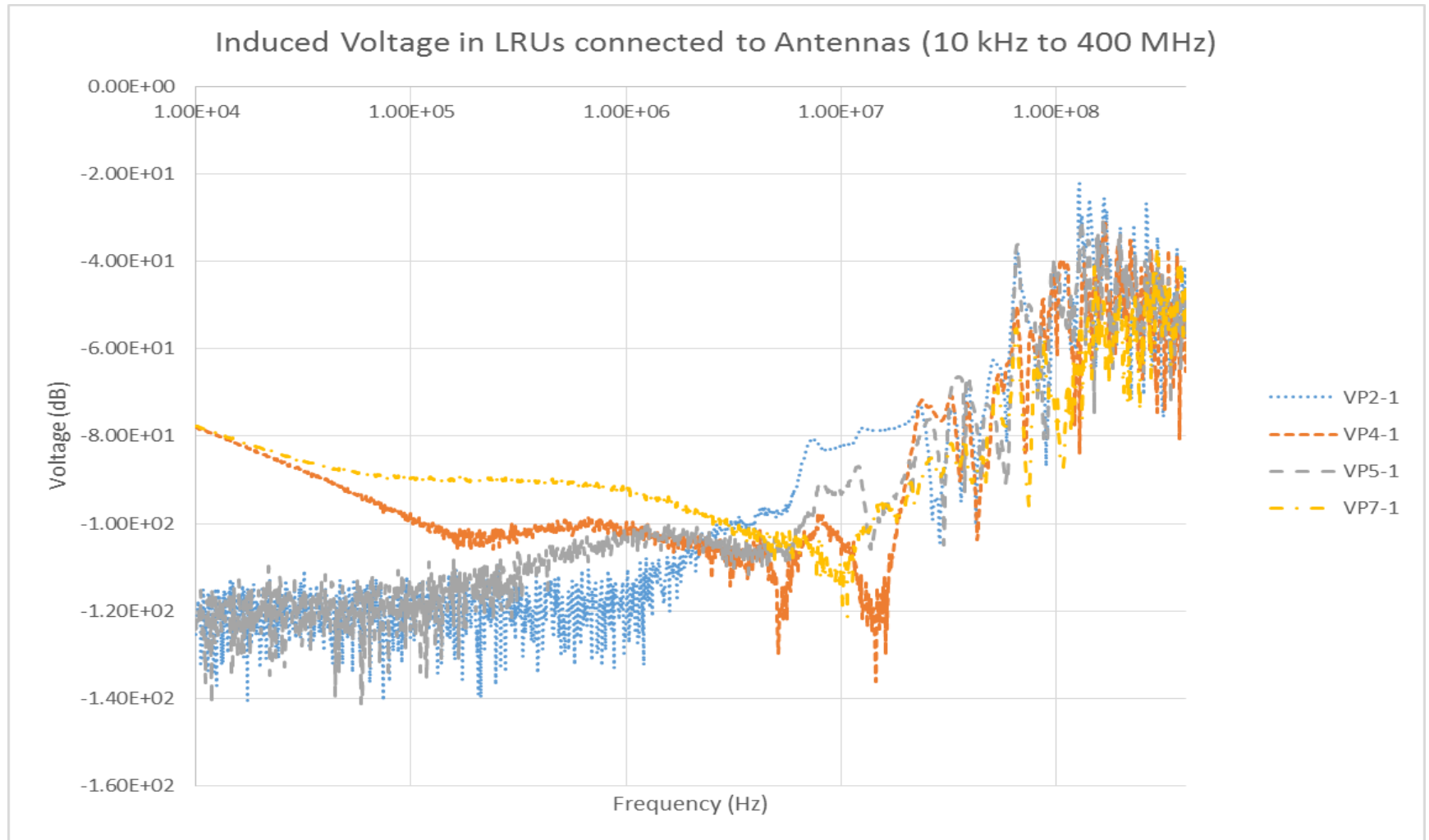


Computed Transfer Function at Test Point V P5-1
(with all bundles in WH8 Short circuited)

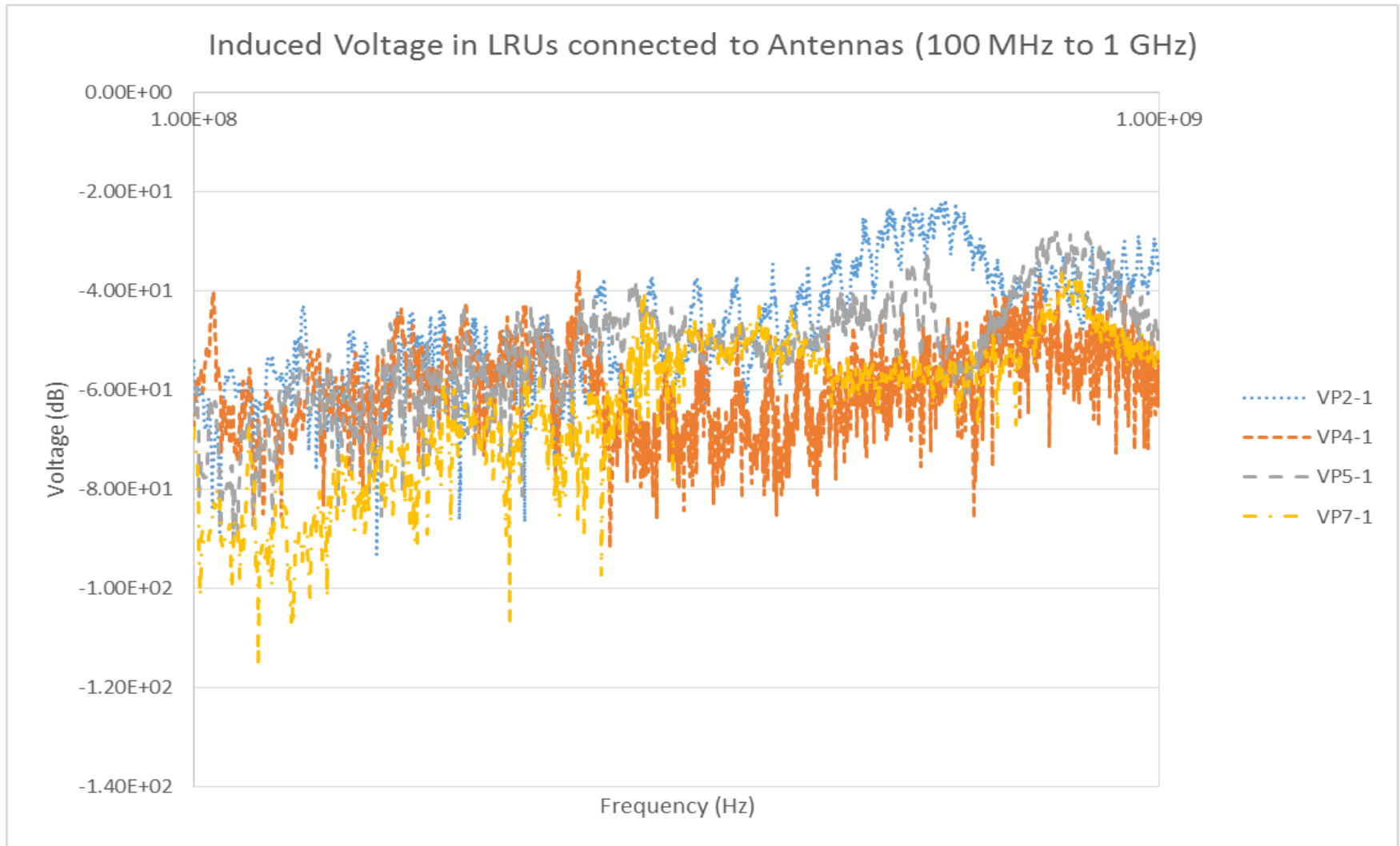


Computed Transfer Function at Test V P 7-1
(with all bundles in WH8 Short circuited)

HIGH INTENSITY RADIATED FIELD EFFECTS

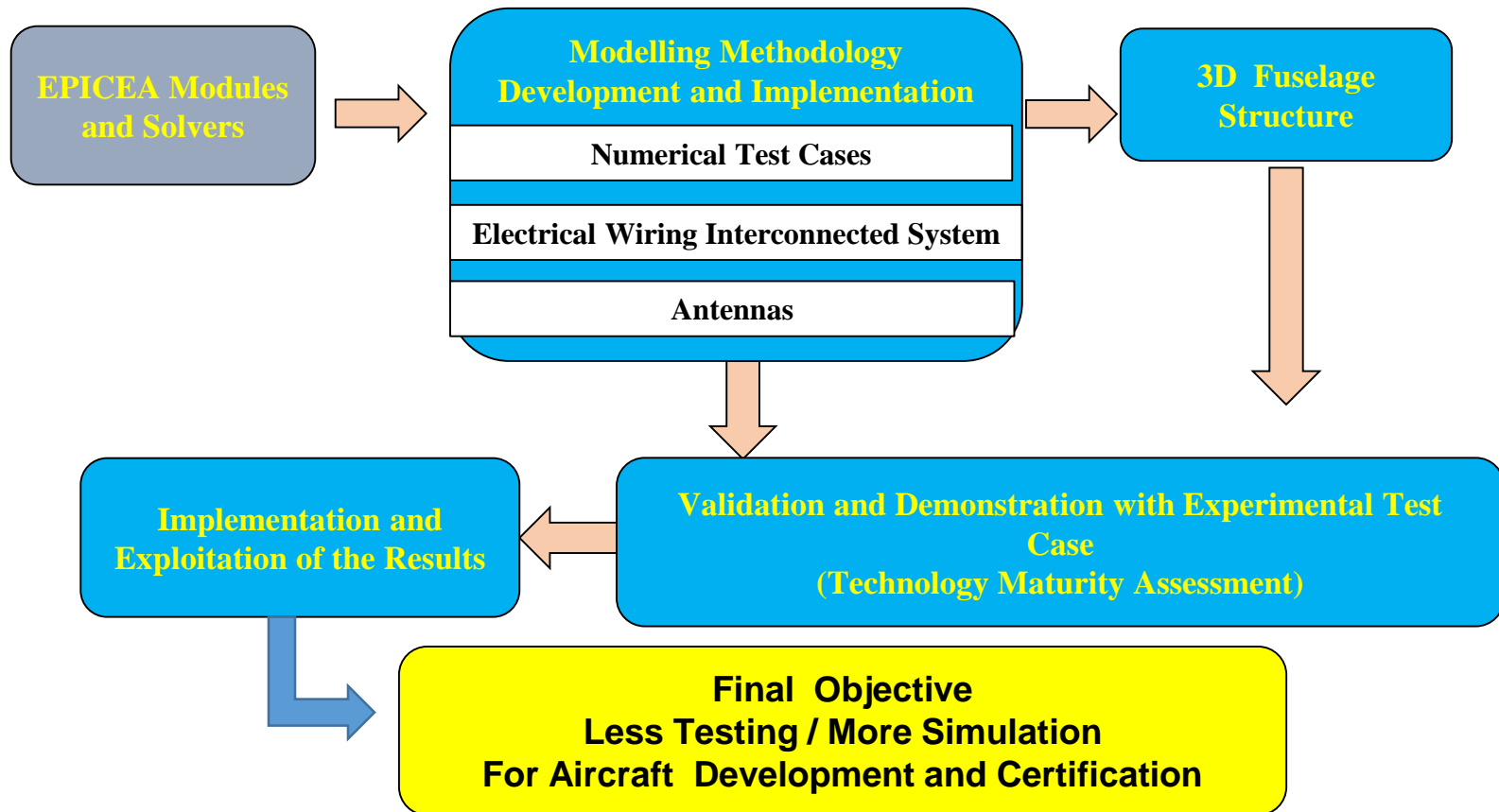


HIGH INTENSITY RADIATED FIELD EFFECTS



CONCLUSION

- ❑ EPICEA is An innovative set of tools to do efficient and simplified electromagnetic modelling for the systems and cabling in composite aircraft



QUESTIONS

